Coordinated Integration of Distributed Energy Resources in Unit Commitment

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Abstract

Distributed energy resources, such as electric vehicles and roof-top solar panels have become increasingly popular and essential components of power distribution systems. However, their growth poses significant challenges to system operation, such as bidirectional power flow, intermittent power generation, increased peak demand, and unexpected frequency/voltage fluctuation. To tackle these challenges, we developed a vehicle-to-grid model, which incorporated dynamic electric vehicles usages, such as driving times, driving distance, and charging/discharging locations. The machine learning method of principal component analysis and XGBoost were used to develop the solar energy prediction model. We also developed a novel unit commitment model to coordinate and aggregate the distributed energy resources in power generation economic dispatch. Electric vehicle charging was used as elastic demand and electric vehicle discharging was used as power generation sources. The solar energy was considered as a negative load. Simulation results showed that uncontrolled electric vehicle charging and solar energy could negatively impact the power systems. For example, the load ramping rate was increased by 384%. Simulation results also showed that the proposed models could mitigate the negative impact and improve energy efficiency. For example, the peak demand, load ramping rate and average generation cost were reduced by 21%, 79%, and 27%.

Keywords: distributed energy resources, unit commitment, solar energy, electric vehicle, vehicle to grid, demand response.

Nomenclature 1 Sets 2 \mathcal{I} The set of EVs 3 4 $\mathcal J$ The set of power generation units \mathcal{T} Time horizon 5 Greek 6 7 α^j, β^i Constant coefficients **8** Symbols and Variables 9 Δt Time interval 10 $\overline{P_l^{\mathrm{EV}}}$ Rated EV charging/discharging power 11 $\overline{p_t^j}$ Maximum power generation limit of the unit j 12 SOC_0 Initial SOC 13 SOC_{max} Maximum SOC SOC_{max} Minimum SOC 14 SOC_{acc} Accepted SOC level at driving times 15 p_t^j Minimum power generation limit of the unit j16 Minimum down time 17 $t_{\rm off}$ 18 $\underline{t_{\mathrm{on}}}$ Minimum up time 19 $B_t^{\mathrm{EV}^i_\downarrow}$ Binary variables indicating EV discharging status 20 $B_t^{\mathrm{EV}^i_{ ightarrow}}$ Binary variables indicating EV driving status 21 $B_t^{\mathrm{EV}^i_\uparrow}$ Binary variables indicating EV charging status 22 $c_i(\cdot)$ Discharging cost of an EV

23	$c_j(\cdot)$	Operation cost of a generation unit
24	$C^{\rm A}_t$	Actual generation cost
25	$C_t^{\rm M}$	Generation cost in an electricity market
26	i, j, k	Index
27	p_t^j	Amount of power generation
28	$p_t^{\mathrm{EV}_\downarrow^i}$	EV discharging power
29	$p_t^{\mathrm{EV}_{\rightarrow}^i}$	EV driving power
30	$p_t^{\mathrm{EV}^i_\uparrow}$	EV charging power
31	$p_t^{\mathrm{EV}^i}$	Power consumption of the i^{th} EV at time slot t
32	$P_{\rm Dri}^{\rm EV}$	Rated EV driving power
33	$R_j^{\rm D}$	Ramping down limit
34	R_j^{U}	Ramping up limit
35	t	Time
36	$t_{i,1}, t_{i,3}$	Departure times of the i^{th} EV
37	$t_{i,2}, t_{i,4}$	Arrival times of the i^{th} EV
38	y_j^t	On/off status of unit j at time t
39	AT	Ambient Temperature
40	PA	Panel Area
41	PE	Panel Efficiency
42	R	Radiation Value
43	SPG	Solar Power Generation
44	Acronyms	

- 45 CCG Combined-Cycle Gas
- 46 DER Distributed Energy Resources
- 47 DR Demand Response
- 48 EV Electric Vehicle
- ⁴⁹ PCA Principal Component Analysis
- 50 SCG Simple-Cycle Gas
- 51 SOC State of Charge
- 52 UC Unit Commitment
- 53 V2G Vehicle-to-Grid
- 54 XGBoost Extreme Gradient Boosting

55 1. Introduction

The worldwide power system transition from the conventional grid to 56 smart grid paradigm is promoting the integration of distributed energy re-57 sources such as roof-top solar, small-scale wind turbines, electrical energy 58 storage systems, electric vehicles (EV), and demand response (DR) [1]. How-59 ever, the growth of distributed energy resources (DER) poses significant chal-60 lenges to the power system operation and control, such as bidirectional power 61 flow, intermittent power generation, increased peak demand, and unexpected 62 frequency/voltage fluctuation [2]. Therefore, DER aggregators and grid op-63 erators need to prepare for high-level distributed energy resource penetration 64 to the power system. 65

Solar and wind energy are intermittent and not economic dispatchable; 66 therefore, accurate short-term forecasting is paramount for their integration. 67 Among other methods such as physical and statistical models, the machine 68 learning method becomes increasingly suitable for short-term renewable en-69 ergy forecasting [3, 4]. However, the appropriate selection of machine learning 70 models and data features remains a significant challenge. A framework to 71 evaluate various machine learning models and feature selection methods was 72 developed in [5], and the best combination to forecast short-term solar power 73 was discovered. 74

Besides accurate forecasting, energy storage systems are also helpful in 75 renewable energy integration into power systems because energy storage can 76 absorb the uncertainty of renewable energy. However, large-scale economic 77 energy storage is not mature yet [6, 7]. Alternatively, as EVs have significant 78 batteries, they can be considered as mobile energy storage with time-varying 79 parameters such as driving distance/period and charging/discharging loca-80 tions [8]. However, uncontrolled EV charging can significantly increase peak 81 demand [9]. 82

To mitigate the challenge of renewable energy and EV integration, they 83 must be included in the power system operation routine, e.g., unit commit-84 ment (UC) that economically dispatches power generation to meet demand 85 [10, 11]. Power system flexibility metrics, e.g., the ramping rate of a load 86 profile, were proposed to assess the flexibility of the power system for re-87 newable energy integration [12]. Energy storage and combined heat & power 88 generation were used in a UC model to compensate the intermittent solar 89 energy [13]. 90

⁹¹ Concentrating solar power technology could also smooth out the variation

of solar energy because it could store energy [14]. The uncertainty in UC 92 model was reviewed in [15]. The security constrained UC model considering 93 the uncertainty of wind generation was developed in [16]. Alternatively, 94 stochastic UC models were developed to cope with the uncertainty from high 95 level penetration of the solar energy [17, 18]. These UC models focused on 96 coping with the uncertainty of solar energy, and the solar energy information 97 was from actual data or predicted by other sources. However, accurate solar 98 prediction models were not integrated into the UC models. 99

EVs are parked 95% of the time on average, and EVs can be controlled 100 to charge or discharge during the parking time, known as the vehicle-to-101 grid (V2G) application [19]. V2G can be incorporated into UC models. For 102 example, a V2G model was developed to analyze the impact of bidirectional 103 flow capacity on power generation dispatch [20]. The EV discharging capacity 104 was used as the spinning reserve in a UC model to absorb the uncertainty 105 from renewable energy [21]. Both the EV charging and discharging in a 106 V2G application were coordinated by a UC model to fill the load valley from 107 renewable energy integration [22]. Furthermore, a security constrained UC 108 model was developed to cope with extreme scenarios of uncertainty from 109 renewable energy and EV penetration [23, 24, 25]. However, these models 110 did not consider dynamic EV usages, such as driving times, driving distance, 111 and plugin locations. 112

UC can be formulated into mixed-integer programming models [26, 27]. Methods have been developed to solve UC models, such as Lagrangian relaxation [28], particle swarm optimization [29, 30, 31] and genetic algorithm [32, 33]. Among others, the mixed-integer linear programming was widely used due to its flexibility, high efficiency, high convergent rate [34, 35, 36, 37, 38, 39, 40].

Nonetheless, highly accurate short-term renewable energy prediction mod-119 els are needed. Also, the dynamic EV usages, such as driving times, driving 120 distance, and plugin locations, need to be modeled. To our best knowledge, 121 UC models with integrated both highly accurate short-term renewable en-122 ergy prediction and the EV dynamic usage have not been developed. In this 123 study, we have developed a highly accurate solar energy prediction model 124 and a V2G model with the dynamic EV usage. A UC model was further 125 developed, which incorporated the solar prediction and V2G models. 126

¹²⁷ The contributions of this work are summarized as follows:

1. A V2G model is developed, in which the dynamic EV usages are mod-

eled, such as driving times, driving distance, and charging/discharging 129 locations. 130

2. A UC model with integrated solar energy prediction and V2G mod-131 els is developed. This model incorporates EV discharging as power 132 generation and controlled EV charging as elastic demand under DR. 133

3. The proposed models can be used to integrate a high level penetration 134 of EV and renewable energy to power systems. 135

The paper is organized as follows. Section II describes the problem for-136 mulation and Section III presents case the simulation results. The discussion 137 is given in Section IV and the conclusion is presented in Section V. 138

2. Problem Formulation 139

The main objective of this study is to economically and reliably integrate 140 DERs including EVs and solar energy into power systems. Fig. 1 shows the 141 system architecture. DER aggregators collect the information from DERs 142 and aggregate DERs to participate in UC. Solar energy is predicted and 143 considered as a negative load in the system. The V2G model incorporates 144 dynamic EV usage. The predicted EV discharging energy is used as power 145 generation in the UC model for economic dispatch. The predicted EV charg-146 ing energy is used as elastic demand under DR. Four conventional genera-147 tors are also used, including coal, combined-cycle gas, simple-cycle gas, and 148 diesel. The developed UC model economically dispatches conventional gener-149 ation units, EV discharging capacity, and EV charging capacity. The major 150 outcomes include reduced generation cost, lower peak demand, lower load 151 variation, and less greenhouse gas emissions. 152

This section presents the dynamic EV usage and V2G model, the solar 153 energy prediction model, and the UC model. 154

2.1. Dynamic EV Usage and V2G 155

A fleet of EVs can be used as a battery bank for power system operation 156 and control. For instance, EV discharging can be used as distributed energy 157 resources, and controlled EV charging can be used as flexible demand in DR. 158 However, this battery bank has dynamic parameters such as driving times, 159 driving distance, and charging/discharging locations. 160

Fig. 2 shows the plug-in and dynamic driving times. Blue color presents 161 EV plug-in periods at homes or workplaces while green color shows driving 162



PCA: principal component analysis, SOC: state of charge, V2G: vehicle-to-grid

Figure 1: System architecture



Figure 2: The diagram of important EV usage times

periods. Throughout the day, there are two driving periods from home t_1 to workplace t_2 and from workplace t_3 to home t_4 . As the daily routine of the people are similar, the values of t_1 , t_2 , t_3 and t_4 tends to be normally distributed [8].

¹⁶⁷ The V2G problem is modeled as follows.

$$p_t^{\mathrm{EV}^i} = p_t^{\mathrm{EV}^i_\uparrow} - p_t^{\mathrm{EV}^i_\downarrow} - p_t^{\mathrm{EV}^i_\to}$$
(1)

$$0 \le p_t^{\mathrm{EV}^i_\uparrow} \le B_t^{\mathrm{EV}^i_\uparrow} \overline{P_l^{\mathrm{EV}}}, \forall i, t \in [t_{i,2}, t_{i,3}] \cup [t_{i,4}, t_{i,1}]$$
(2)

$$0 \le p_t^{\mathrm{EV}_{\downarrow}^i} \le B_t^{\mathrm{EV}_{\downarrow}^i} \overline{P_l^{\mathrm{EV}}}, \forall i, t \in [t_{i,2}, t_{i,3}] \cup [t_{i,4}, t_{i,1}]$$
(3)

$$p_t^{\mathrm{EV}_{\rightarrow}^i} = B_t^{\mathrm{EV}_{\rightarrow}^i} P_{\mathrm{Dri}}^{\mathrm{EV}}, \forall i, t \in [t_{i,1}, t_{i,2}] \cup [t_{i,3}, t_{i,4}]$$

$$\tag{4}$$

$$B_t^{\mathrm{EV}^i_{\uparrow}}, B_t^{\mathrm{EV}^i_{\downarrow}}, B_t^{\mathrm{EV}^i_{\rightarrow}} \in \{0, 1\}$$

$$\tag{5}$$

$$B_t^{\mathrm{EV}^i_\uparrow} + B_t^{\mathrm{EV}^i_\downarrow} + B_t^{\mathrm{EV}^i_{\rightarrow}} \le 1 \tag{6}$$

$$\operatorname{SOC}_{i,ts} = \operatorname{SOC}_0 + \sum_{t=0}^{\iota s} p_t^{\operatorname{EV}^i} \Delta t, \quad \forall i$$
 (7)

$$SOC_{min} \le SOC_{i,ts} \le SOC_{max}, \quad \forall i, t$$
 (8)

$$\operatorname{SOC}_{i,t_1} \ge \operatorname{SOC}_{\operatorname{acc}}, \quad \forall i$$

$$\tag{9}$$

$$\operatorname{SOC}_{i,t_3} \ge \operatorname{SOC}_{\operatorname{acc}}, \quad \forall i$$
 (10)

where $p_t^{\text{EV}^i}$ is the power consumption of the i^{th} EV at time slot t. $p_t^{\text{EV}^i_{\uparrow}}, p_t^{\text{EV}^i_{\downarrow}}$ and $p_t^{\text{EV}^i_{\rightarrow}}$ are the EV power consumption of charging, discharging and driving respectively. $B_t^{\text{EV}^i_{\uparrow}}, B_t^{\text{EV}^i_{\downarrow}}$ and $B_t^{\text{EV}^i_{\rightarrow}}$ are binary variables indicating EV status ¹⁷¹ of charging, discharging and driving respectively. For example, $B_t^{\text{EV}^i_{\uparrow}} = 1$ ¹⁷² indicates EV charging and $B_t^{\text{EV}^i_{\uparrow}} = 0$ indicates no EV charging.

Eq. (2) shows that the EVs can be charged with the power between 0 and rated charging power when they are at homes or workplaces. $t \in [t_{i,2}, t_{i,3}] \cup$ $[t_{i,4}, t_{i,1}]$ is the time period when the i^{th} EV is at homes or workplaces. This time is different among EVs. Likewise, Eq. (3) shows the EV discharging constraint when they are at homes or workplaces. Eq. (4) is the power consumption during the driving period.

Eq. (5) shows that $B_t^{\mathrm{EV}_{\uparrow}^i}, B_t^{\mathrm{EV}_{\downarrow}^i}, B_t^{\mathrm{EV}_{\downarrow}^i}$ are binary variables. Eq. (6) shows the EV cannot be charging, discharging and driving simultaneously.

Eq. (7) shows the SOC of the i^{th} EV at t, where Δt is the time duration of each interval. Eq. (8) is a constraint for limiting the individual EV's SOC between the minimum and maximum limit of SOC, e.g., 0% and 100%. Eq. (9) and Eq. (10) constraints the SOC at start of driving times (t_1 and t_3), which indicates that the EV should have sufficient energy for driving.

This V2G model is incorporated into the UC model discussed in Section 2.3.

188 2.2. Solar Prediction

Solar energy prediction is paramount in power system operation since so-189 lar energy is intermittent and generally non-dispatchable. Machine learning 190 algorithms play an important role in solar energy prediction. Our earlier 191 research in [5] showed that the combination of principal component analysis 192 (PCA) and XGBoost provided the most accurate prediction among others: 193 PCA with random forest, PCA with neural networks, feature importance 194 with XGBoost, feature importance with neural networks, and feature impor-195 tance with random forest. 196

Therefore, this study uses PCA and XGBoost for solar energy prediction. Specifically, we use PCA for feature selection and use XGBoost to map the selected features to solar radiation signals. To train the predictive model, we use the weather data in the period of September-December, 2016, from the Kaggle database [41]. The data includes 11 attributes such as date, time, radiation, temperature, etc.

²⁰³ The following steps are carried out [5].

Step 1. Data pre-processing: 1) The data are cleaned. 2) The time and date are extracted from the UNIX time. 3) The sunset and sunrise times are used to extract the length of the daytime. 4) The data are divided into threedata sets: training, cross-validation, and test.

Step 2. Manual feature selection: By using statistical methods, the attributes are ordered based on the correlations with solar radiation. The most seven correlated attributes are selected: temperature, humidity, pressure, wind direction, wind speed, day, and time.

Step 3. PCA for feature selection: PCA is used to reduce the seven attributes into four components.

Step 4. XGBoost to map the selected features to solar radiation signals:
XGBoost is a machine learning algorithm based on a sequential ensemble of
decision trees, where weak learners can learn jointly to build a strong learner.
The training and cross-validation datasets are used to train the parameters and hyperparameters. For example, the number of trees, maximum
depth of trees, and step size were tuned as 70, 13, and 0.05, respectively.
The final test using the test dataset shows 99.4% accuracy.

Finally, the predicted solar radiation is used to estimate the solar power generation, which is calculated as follows.

$$SPG = PE \cdot PA \cdot R \cdot [1 - 0.005(AT - 25)]$$
(11)

where PE is the panel efficiency, and PA is the panel area. R is the radiation value, while AT is the ambient temperature. SPG represents solar power generation.

The predicted solar energy is considered a negative demand and incorporated into the UC model discussed in the next section.

226 2.3. Unit Commitment Model with V2G and Solar Prediction

UC is used to economically dispatch generation units to meet demand. Unlike a conventional UC model, the proposed model incorporates the V2G model and solar energy prediction. EV discharging is used as power generation units, and EV charging is used as an elastic load under the concept of DR. The predicted solar energy is used as a negative load.

$$\underset{p_t^j, p_t^{\mathrm{EV}_{\downarrow}^i}, p_t^{\mathrm{EV}_{\uparrow}^i}}{\operatorname{minimize}} \quad \sum_{t \in \mathcal{T}} \left[\sum_{j \in \mathcal{J}} c_j(p_t^j) + \sum_{i \in \mathcal{I}} c_i(p_t^{\mathrm{EV}_{\downarrow}^i}) \right]$$
(12)

232 subject to:

$$\sum_{j \in \mathcal{J}} p_t^j + \sum_{i \in \mathcal{I}} p_t^{\mathrm{EV}_{\downarrow}^i} = p_t^d - p_t^s + \sum_{i \in \mathcal{I}} p_t^{\mathrm{EV}_{\uparrow}^i}, \ \forall t \in \mathcal{T}$$
(13)

$$y_t^j \in \{0, 1\}, \quad \forall t \in \mathcal{T}, j \in \mathcal{J}$$
 (14)

$$\underline{p_t^j} y_t^j \le p_t^j \le \overline{p_t^j} y_t^j, \quad \forall t \in \mathcal{T}, j \in \mathcal{J}$$
(15)

$$R_j^{\mathrm{U}} \le p_j^t - p_j^{t-1} \le R_j^{\mathrm{D}}, \quad \forall t \in \mathcal{T}, j \in \mathcal{J}$$
 (16)

$$y_t^j - y_{t-1}^j \le y_k^j \quad \forall j \in \mathcal{J}, t \in \{2 \dots |\mathcal{T}| - 1\}, \\ k \in \{\min\left(t + \underline{t_{\text{on}}} - 1, |\mathcal{T}|\right)\}$$

$$(17)$$

$$y_{t-1}^{j} - y_{t}^{j} \leq 1 - y_{k}^{j} \quad \forall j \in \mathcal{J}, t \in \{2 \dots |\mathcal{T}| - 1\},$$
$$k \in \left\{\min\left(t + \underline{t_{\text{off}}} - 1, |\mathcal{T}|\right)\right\}$$
(18)

Eq. (1) - (10)

The objective function is to minimize the generation cost. \mathcal{T} is the set of EV plug-in times. \mathcal{J} is the set of power generation units. p_t^j and $c_j(\cdot)$ is the power generation and cost of the j^{th} power unit, which is defined as follows:

$$c_j(p_t^j) = \alpha^j p_t^j \tag{19}$$

where α^j is constant.

 \mathcal{I} is the set of EVs. $c_i(\cdot)$ is the discharging cost of the i^{th} EV, which can be defined as follows.

$$c_i(p_t^{\mathrm{EV}_{\downarrow}^i}) = \beta^i p_t^{\mathrm{EV}_{\downarrow}^i} \tag{20}$$

where β^i is constant.

The decision variables include $p_t^j, p_t^{\mathrm{EV}_{\downarrow}^i}$ and $p_t^{\mathrm{EV}_{\uparrow}^i}$. Although EV charging $(p_t^{\mathrm{EV}_{\uparrow}^i})$ is not in the objective function, it is flexible load under DR shown in Eq. (13).

Eq. (13) is the power balance constraint between power generation and demand. p_t^d is a reference load at time t. We define the reference load as the load profile without EV and solar energy penetration. p_t^s represents the solar power at time t. The power are from the power generation units (p_t^j) and EV discharging. The demand includes the net load $(p_t^d - p_t^s)$ and the flexible EV charging load. In Eq. (14) y_j^t is a binary variable, which is the on/off status of unit jat time t. In Eq. (15), $\overline{p_t^j}$ represents the maximum power generation limit of the unit j and \underline{p}_t^j is the minimum power generation that the unit j needs to produce once it is on due to physical constraints. Eq. (16) exhibits the ramping up/down constraint of the unit j, where R_j^U and R_j^D show ramping up and down limit respectively.

Eq. (17) is the minimum on-time constraint, which means that the power generation unit has to remain on for a minimum time $\underline{t_{on}}$ after it is switched on due to economical reasons or mechanical design limits. Similarly, as observed in Eq. (18), a unit has to remain off for a minimum time $\underline{t_{off}}$ after it is switched off. $|\mathcal{T}|$ is the cardinality of the set \mathcal{T} .

256 3. Simulation Results and Analysis

To evaluate the proposed models, cases studies were conducted in 3 scenarios:

- ²⁵⁹ 1. Reference scenario: no EV nor solar energy penetration
- 260 2. Uncontrolled EV and solar energy penetration
- $_{261}$ 3. V2G and solar energy penetration with 30% EVs penetration
- $_{262}$ 4. V2G and solar energy penetration with 80% EVs penetration

263 3.1. Experimental Setup

This study simulated a power system having 300 homes. We first deter-264 mined the energy consumption of the simulated power system as follows. The 265 electricity usage can be grouped as residential, industrial, and commercial 266 sectors, while the residential sector consumes 1/3 of total electricity [42, 43]. 267 Furthermore, the average electricity usage per household is 30 kWh/day [44]. 268 Therefore, the energy consumption of the simulated power system was calcu-269 lated as $0.03 \text{ MWh} \times 300 \times 3 = 30 \text{ MWh}$. The load profile from PJM [45] was 270 used and scaled down to fit the magnitude of our simulation. Fig. 3 shows 271 the scaled load profile, and we denote it as the reference load profile in this 272 study. 273

Table 1 summarizes the parameters for the V2G model. We assumed that 30% of the consumers have EVs; therefore, 90 EVs were considered. The start EV driving times follow a normal distribution, and the expected value μ and the standard deviation σ are shown in the table. The driving time period was assumed as 45 minutes [8]; therefore $t_2 = t_1 + 45$ and $t_4 = t_3 + 45$. The



Figure 3: The reference load profile (Scaled from the actual load profile on October 27, 2019 from PJM. [45])

rated power $(\overline{P_l^{\text{EV}}})$ of EV charging/discharging was 3.3 kW at both home and workplace. The rated power for EV driving $(P_{\text{Dri}}^{\text{EV}})$ was 8 kW. In addition, the EV battery capacity was 50 kWh, and the initial SOC was 50%. The maximum and minimum SOC were 0% and 100%.

The solar model discussed in Section II.B was used to predict the solar energy based on the weather data in [41]. We assumed that 20% of homes have roof-top solar, and 10 kW PV system was designed with overall 70% system efficiency. The total PV area per home roof-top was 87 m^2 with PV panel efficiency of 16%. Eq. 11 was used to calculate the solar power generation. Table 2 shows the parameters. Fig. 4 shows the predicted solar power.

Table 3 summarizes the parameters of the UC model for conventional power generation units: coal (j = 1), combined-cycle gas (j = 2), simplecycle gas (j = 3) and diesel (j = 4). The combined-cycle gas units use both gas-turbine and heat recovery steam-turbine and therefore are more efficient than simple-cycle gas units. However, simple-cycle gas units have the advantages of quick start and high ramping rate.

We also considered the power generation dispatch in an electricity mar-

Parameter	Values
$\beta^i, \forall i \in \mathcal{J}$	\$50/MWh
t_1 (normal distribution)	$\mu = 7:00 \text{ and } \sigma = 1 \text{ hour } [8, 9]$
t_3 (normal distribution)	$\mu = 17:00 \text{ and } \sigma = 2.8 \text{ hours } [8, 9]$
$ \mathcal{T} $	24 hours
Time Interval	5 minutes
$\overline{P_l^{\text{EV}}}$	3.3 kW [8]
$P_{\rm Dri}^{\rm EV}$	8 kW
SOC_{min}	0%
SOC_{max}	100%
SOC_{acc}	50%

Table 1: Major Parameters for V2G Model

Table 2: Parameters for Solar P	rediction
Parameter	Values
Rated Solar Power per home	10 kW
Ambient Temperature	$28 C^o$
PV Efficiency (PE)	16%
System Efficiency	70%
PV Area (PA)	$87 m^2$



Figure 4: Predicted solar power

ket. The electricity market is cleared when the power generation units are dispatched to meet the demand. All the dispatched generation units are paid the same as the generation unit with the highest generation cost. The market-based generation cost was calculated as follows.

$$C_t^{\rm M} = \max\left[c_j(p_t^j)\right] \tag{21}$$

The proposed optimization models were solved by the CVX with the Gurobi solver [46, 47, 48].

298 3.2. Scenario #1: Reference Scenario

The reference scenario did not consider the integration of solar energy and EVs. The UC model without V2G was solved to dispatch the four power units.

Fig. 5 shows the economic dispatch of the four power generation units, where the area plots show the power production of the units, and the envelope shows the total generation. The generation must always meet the demand. The energy consumption was 30 MWh. The total generation cost was \$1538. The average generation cost was 1538/30 = \$51.3/MWh.

Parameter	Coal	CCG	SCG	Diesel
α^j (\$/MWh)	28.1	30.2	45	62
$\overline{p_t^j}$ (kW)	750	400	400	1000
p_t^j (kW)	10	4	2	0
$\overline{t_{\rm on}}$ (minutes)	30	10	20	5
$\overline{t_{\text{off}}}$ (minutes)	15	10	20	5
$\overline{R_i^{U}}$ (kWh/5-min)	0.5	2	4	100
$R_i^{\rm D}$ (kWh/5-min)	-0.5	-2	-4	-100

Table 3: Major Parameters of the UC Model

CCG: Combined-Cycle Gas. SCG: Simple-Cycle Gas

The peak demand and the variance of the reference load were 1478.1 kW and 22237.0 kW, respectively. The maximum ramping rate was 13.9 kWh/5-min.

310 3.3. Scenario #2: Uncontrolled EV and solar energy penetration

To evaluate the impact of uncontrolled EV charging and solar energy penetration on the power system, three sub-scenarios were designed: #2A uncontrolled EV charging penetration, #2B - solar energy penetration, and #2C - both uncontrolled EV charging and solar energy penetration.

The blue line in Fig. 6 shows the load profile in Scenario #2A. The peak demand and the variance of the load profile were 1741.7 kW and 42939.0 kW, respectively. The maximum ramping rate 67.3 kWh/5-min. The energy consumption was 32 MWh. The generation cost was \$1698. The average generation cost was \$53.1/MWh.

The red line in Fig. 6 shows the net load profile in the case of solar energy penetration. The predicted solar power is shown in Fig. 4 acts as a negative load. The peak demand and the variance of the load profile were 1477.4 kW and 37529.0 kW, respectively. The energy consumption was 26.4 MWh. The generation cost was \$1398. The average generation cost was \$52.9/MWh

Fig. 7 shows the reference load profile and the net load profile with both uncontrolled EV and solar penetration. With both uncontrolled EV and solar penetration, the peak demand and the variance of the load profile were 1741.0 kW and 82699.0 kW, respectively. The energy consumption was 28.4 MWh. The generation cost was \$1554. The average generation cost was \$54.9/MWh.



Figure 5: Power generation of different units in Scenario #1



Figure 6: Load profiles of Scenario #2A and #2B



Figure 7: Load profiles of Scenario #1 and #2C

Fig. 8 shows the economic dispatch of the four power generation units for Sub-scenario #2C.

The intermittent solar energy can significantly increase the net load ramping rate, which can pose a significant challenge for power system operation. The maximum ramping rate was 67 kWh/5-min for Scenario #2B and #2C. The ramping rate was increased by 384% compared with Scenario #1.

336 3.4. Scenario #3: V2G and solar energy penetration

In this scenario, the UC model with V2G was applied in the case with both EV and solar penetration. EV charging was included as flexible demand and EV discharging was included as power generation in the UC model. Eq. 20 was used to calculate the EV discharging cost.

Fig. 9 shows the load profiles of Scenario #2C and #3. As can be seen, the peak demand was reduced from 1741.0 kW to 1376.6 kW and the variance of the load profile was reduced from 82699.0 to 16808.0 kW. The maximum ramping rate was reduced from 67.4 kWh/5-min to 14.1 kWh/5-min. Fig. 10 shows uncontrolled EV charging and the EV charging and discharging curves under V2G. Blue line shows the uncontrolled EV charging as the reference. Red line shows the aggregated EV charging/discharging curves under V2G,



Figure 8: Power generation of different units in Scenario $\#2\mathrm{C}$



Figure 9: Load profiles of Scenario #2C and #3



Figure 10: Uncontrolled EV charging curve (Scenario #2C) and EV charging and discharging curve with V2G (Scenario #3)

where positive values were EV charging and negative values were EV dis-348 charging. As can be seen, the EVs were under charging during the load 349 valley period. This is the period when there is plenty of solar energy avail-350 able. By contrast, EVs were under discharging during the peak demand 351 period. Fig. 11 shows the economic dispatch of the four power generation 352 units in the Scenario #3. The EV discharging energy was not shown in the 353 area plot but it acted as a negative load similar to the solar energy. The 354 energy consumption was 27.1 MWh. The generation cost was \$1098. The 355 average generation cost was \$40.1/MWh. 356

357 3.5. Scenario #4: V2G and solar energy penetration with 80% EVs penetra-358 tion

In Scenario #4, to further investigate the flexibility of the UC model with V2G (solar and EV penetration), we increased the EV penetration to 80%. Half of the EVs were charged with 3.3 kW chargers, and the rest of the EVs were with 9.6 kW chargers.

Fig. 12 shows the load profiles of uncontrolled EV charging and EV charging and discharging curve with V2G. The blue line represents the load profile



Figure 11: Power generation of different units in Scenario #3



Figure 12: Uncontrolled EV charging curve and EV charging and discharging curve with V2G in Scenario #4

#	Peak Demand	Load Variance	Max Ramping
	kW	kW	kWh/5-mins
#1	1478.1	22237.0	13.9
#2A	1741.7	42939.0	67.3
	$(18\%\uparrow)$	$(98\%\uparrow)$	$(384\% \uparrow)$
#2B	1477.4	37529.0	29.1
	(0%)	$(69\% \uparrow)$	$(109\% \uparrow)$
#2C	1741.0	82699.0	67.4
	$(18\%\uparrow)$	$(272\% \uparrow)$	$(384\% \uparrow)$

Table 4: Major observations in three SubScenarios of Scenario #2

with the uncontrolled EV charging, and the red line shows the EV charging and discharging curve with the V2G application. With uncontrolled EV charging, the peak demand and load profile variance were 2767 kW and 333990 kW, respectively. The proposed UC model with V2G reduced the peak demand by 43% to 1590 kW. It also reduced the load profile variance by 92% to 26872 kW.

371 4. Discussion

In this study, we have developed a V2G model and a machine learning 372 model for solar energy prediction. We also develop a UC model that in-373 corporates the V2G and solar energy prediction model. In the UC model, 374 EV discharging is used as power generation, and EV charging is used as a 375 flexible demand in DR. The predicted solar energy is considered a negative 376 load. Experiments are designed in four scenarios to evaluate the proposed 377 models. For a demonstration purpose, we only considered small scale power 378 generation units, and a small number of EVs, and small scale solar energy 379 generation. However, the proposed model is readily to be scaled up. 380

Table 4 summarizes the simulation results in Scenario #2. The results 381 show that uncontrolled EV charging and solar energy can negatively impact 382 the power system. For example, uncontrolled EV charging can increase the 383 peak demand by 18%, if 30% of householders have EVs. To meet the in-384 creased peak demand, utilities may need to build new power plants, which 385 requires significant investment. Solar energy can also negatively impact the 386 power system because solar energy is not economically dispatchable and inter-387 mittent. For instance, if 20% of householders install solar panels, solar power 388

#	Peak Demand	Load Variance	Max Ramping	AGC
	kW	kW	kWh/5-mins	\$/MWh
#2C	1741.0	82699.0	67.4	54.9
#3	1376.6	16808.0	14.1	40.1
	$(21\%\downarrow)$	(80% ↓)	$(79\% \downarrow)$	$(27\%\downarrow)$

Table 5: Major observations in Scenario #2C and #3

AGC: A	Average	Generation	Cost.
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can increase the load ramping rate by 109%. To meet the higher ramping 389 load, less efficient power generators must be used, e.g., simple-cycle gas tur-390 bines or diesel generators. The usage of inefficient generators will produce 391 more greenhouse gases and decrease the value of solar energy. Furthermore, 392 as shown in Scenario #2C the negative impact can be superimposed with 393 both EVs and solar energy penetration. As the current solar power gen-394 eration cost is not viable comparing with conventional generators, it is not 395 fair to compare the total generation cost between Scenario #1 and #2. We 396 therefore do not compare the generation cost between Scenario #1 and #2. 397

Table 5 summarized the simulation results of Scenario #2C and #3. As 398 can be seen, the proposed method can mitigate the negative impact of so-390 lar and uncontrolled EV penetration. Furthermore, the proposed model can 400 incorporate V2G applications to reduce peak demand, flatten load profile, 401 reduce generation cost, and improve energy efficiency. Specifically, the peak 402 demand is reduced by 21%. The load variance and load ramping are de-403 creased by 80% and 79%, respectively. Furthermore, the average generation 404 cost is reduced by 27%. Furthermore, in the case of 80% of EV penetra-405 tion, the proposed UC model with V2G reduced the peak demand and load 406 profile variance by 43% and 92%, respectively, compared with uncontrolled 407 EV charging. The improvement can avoid new infrastructure investment be-408 cause of the reduced peak demand. Renewable energy integration and EV 409 incorporation can also reduce greenhouse gas emissions. 410

411 5. Conclusion

The penetration of DERs poses significant challenges to power system operation. However, proper management of them can also provide benefits. To tackle the challenges and reveal the benefits, we have developed a V2G model and a solar energy prediction model. We also developed a UC model that

incorporates the V2G and solar energy prediction models. Simulation results 416 showed that uncontrolled EV charging and solar energy could negatively im-417 pact the power systems. For example, if 30% of the households have EVs and 418 20% of households install solar panels, the peak demand and ramping rate of 419 the load profile would be increased by 18% and 384%, respectively. It may 420 require building new power plants to meet the increased peak demand and 421 using less efficient power plants to meet the increased load variation. The 422 proposed UC model could economically dispatch EV discharging and use EV 423 charging as a flexible demand to mitigate the negative impact and improve 424 energy efficiency. For instance, the peak demand, ramping rate of the load 425 profile, and average generation cost were reduced by 21%, 79%, and 27%. 426 The proposed models can be used to quantitatively evaluate the impact of 427 EVs and solar energy on the power systems with different penetration levels. 428 Through the evaluation, grid operators can visualize the impact and prepare 420 for the penetration based on their situation. The proposed UC and V2G 430 models can also efficiently and economically integrate EVs and solar energy 431 into power systems. Specifically, the proposed models can reduce generation 432 costs, delay infrastructure investments, and reduce greenhouse gas emissions. 433

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